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OF PIEZOELECTRIC MACROFIBER COMPOSITES**

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NONLINEAR ELECTROMECHANICAL FIELDS AND LOCALIZED POLARIZATION SWITCHING OF PIEZOELECTRIC MACROFIBER COMPOSITES

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This paper examines theoretically and experimentally the nonlinear electromechanical response of piezoelectric macrofiber composites. 3D finite element analysis was carried out to study the strain versus electric field curve and the internal electromechanical fields near interdigitated electrodes in the macrofiber composites by introducing a model for polarization switching. The piezoelectric fibers in the macrofiber composite are partially or fully poled. Results on the strain versus electric field curves from microelectromechanical models and simple experiments were also presented, and comparison was made with the finite element solutions.

1. Introduction

Piezoelectric macrofiber composite (MFC) elements, developed at NASA Langley Research Center for aerospace applications, are gaining increasing interest for applications in structural health monitoring [Brunner et al. 2009] and energy harvesting [Song et al. 2009] systems. The development of the MFC helps to overcome some of the limitations of conventional lead zirconate titanate (PZT) ceramics, especially brittleness, lack of reliability, and conformability. In [Williams et al. 2006] the actuation behavior of MFC under electromechanical loading was investigated analytically and experimentally, and the piezoelectric and electrostrictive coefficients were discussed. Also, in [Bilgen et al. 2010] the structural response of MFC actuated clamped-free thin cantilever beams was studied.

In some MFC applications, high values of stress and electric fields arise in the neighborhood of electrode tips in PZT fibers, and the field concentrations can result in electromechanical degradation [Shindo et al. 2004; Narita et al. 2007]. There is also another problem related to the manufacturing process. A PZT wafer is first diced into rectangular fibers. This fiber arrangement is infiltrated with resin and cured together with interdigitated Kapton electrode sheets in a high-precision lamination pressing machine. After this, in a final step, the MFC is polarized with high voltages for about 10 minutes at room temperature. With these fabrication techniques, the resulting polarization of the PZT fibers will inevitably be partial. Due to the presence of interdigitated electrode (IDE) edges and the resulting inhomogeneity of the constituents, piezoelectric MFCs can suffer damage prematurely during service. It is therefore important to understand electromechanical field concentrations near IDEs in piezoelectric MFCs.

In this paper, we investigate the electromechanical response of piezoelectric MFCs. Recent works [Dano and Jullière 2007; Deraemaeker et al. 2009] used the linear constitutive relations for coupling

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response in MFCs; hence the novelty of this work consists of exploration of the nonlinear behavior during the polarization switching process and comparison of the numerical values with the experimental data. In Section 2, the basic equations for piezoelectric materials are described. A nonlinear 3D finite element model incorporating the polarization switching mechanism is also presented to predict the strain versus electric field curve and internal electromechanical fields near IDEs in piezoelectric MFCs. The piezoelectric fibers in the MFC are partially or fully poled. In addition, the effective longitudinal piezoelectric constant of the MFC with fully poled PZT fibers is derived analytically using microelectromechanical models. In Section 3, the electric field-induced strain is measured. Test results on the strain versus electric field curve are compared to predictions in Section 4. The finite element results on the internal electromechanical fields are then discussed. Our conclusions are summarized in Section 5.

2. Analysis

2.1. Basic equations. Consider a piezoelectric material with no body force and free charge. The governing equations in the Cartesian coordinates x_i ($i = 1, 2, 3$) are

$$\sigma_{ji,j} = 0, \quad D_{i,i} = 0, \quad (1)$$

where σ_{ij} is the stress tensor, D_i is the electric displacement vector, a comma denotes partial differentiation with respect to the coordinate x_i , and Einstein summation convention over repeated indices is used. The relation between the strain tensor ε_{ij} and the displacement vector u_i is given by

$$\varepsilon_{ij} = \frac{1}{2}(u_{j,i} + u_{i,j}), \quad (2)$$

and the electric field intensity vector is $E_i = -\phi_{,i}$, where ϕ is the electric potential. In a ferroelectric material, domain switching leads to changes in the remanent strain ε_{ij}^r and remanent polarization P_i^r . The constitutive relations can be written as

$$\sigma_{ij} = c_{ijkl}(\varepsilon_{kl} - \varepsilon_{kl}^r) - e_{kij}E_k, \quad D_i = e_{ikl}(\varepsilon_{kl} - \varepsilon_{kl}^r) + \epsilon_{ik}E_k + P_i^r. \quad (3)$$

In (3), c_{ijkl} and e_{ikl} are the elastic and piezoelectric tensors, and ϵ_{ik} is the dielectric permittivity tensor. Valid symmetry conditions for the material constants are

$$c_{ijkl} = c_{jikl} = c_{ijlk} = c_{klij}, \quad e_{kij} = e_{kji}, \quad \epsilon_{ik} = \epsilon_{ki}. \quad (4)$$

The constitutive equations (3) for piezoelectric material poled in the x_3 -direction are found in Appendix A.

Although there are many criteria that can be used to predict polarization switching in piezoelectric materials, we choose the switching criterion proposed in [Hwang et al. 1995]. This is due to the fact that the model is simple and quite successful at predicting the homogeneous average response of PZT material systems [Steinkopff 1999; Hayashi et al. 2003]. In this model, the direction of a spontaneous polarization P^s of each grain can change by 90° or 180° for ferroelectric switching induced by a sufficiently large electric field. 90° ferroelastic switching is induced by a sufficiently large stress field. This criterion requires that a polarization switches when the combined electrical and mechanical work exceeds a critical value; that is,

$$\sigma_{ij}\Delta\varepsilon_{ij} + E_i\Delta P_i \geq 2P^s E_c, \quad (5)$$

where E_c is a coercive electric field, and $\Delta\varepsilon_{ij}$ and ΔP_i are the changes in the spontaneous strain and spontaneous polarization during switching, respectively. The values of $\Delta\varepsilon_{ij}$ and ΔP_i are given in Appendix B. The constitutive equations (3) after polarization switching are given by

$$\sigma_{ij} = c_{ijkl}(\varepsilon_{kl} - \varepsilon_{kl}^r) - e'_{kij}E_k, \quad D_i = e'_{ikl}(\varepsilon_{kl} - \varepsilon_{kl}^r) + \epsilon_{ik}E_k + P_i^r. \quad (6)$$

The new piezoelectric constant e'_{ikl} is given in Appendix C.

2.2. Model. Consider a M-4010-P1 MFC (Smart Material Corp., Sarasota, FL) with overall dimensions of about 50 mm \times 22 mm \times 0.3 mm. The MFC is comprised of very thin PZT-5A fibers (width $2w_p$, thickness $2h_p$) that are unidirectionally aligned in an epoxy matrix and sandwiched between two sets of copper IDE (width $2w_e$, thickness h_e) patterns as shown in Figure 1a. The IDE patterns are printed on a Kapton film (thickness h_k). The MFC has an IDE spacing of about 0.5 mm and has an active area of about 40 mm \times 10 mm. The material characteristics of PZT-5A are listed in Table 1, and the coercive electric field is approximately $E_c = 1.5$ MV/m. The Young's modulus E and Poisson's ratio ν of the epoxy, copper, and Kapton are listed in Table 2 [Deraemaeker et al. 2009].

Figure 1b illustrates the repeating unit of the MFC. A rectangular Cartesian coordinate system $O-xyz$ is used with the z -axis coinciding with the PZT fiber direction. The repeating unit of the MFC occupies the region ($0 \leq x \leq W$, $0 \leq y \leq H$, $0 \leq z \leq L$). The model consists of rectangular PZT fiber (width w_p , length L) embedded in an epoxy matrix and Kapton film (width W , length L). Electrodes 1 and 3 of area $W \times w_e$ and electrode 2 of area $W \times 2w_e$ are also incorporated into the model. The total thickness of the model is $H = h_p + h_e + h_k$.

With the IDEs, the electric field E_0 is applied along the PZT fibers (the z -direction) which produces much higher in-plane actuation strain ε_0 than traditional monolithic PZT poled through-the-thickness (see Figure 2) [Bent and Hagood 1997; Williams et al. 2004; Paradies and Melnykowycz 2007]. We consider the following electrical boundary conditions: the electric potentials on the interface between the PZT fiber and electrode 1 (that is, $0 \leq x \leq w_p$, $y = h_p$, $0 \leq z \leq w_e$) and the interface between the PZT fiber and electrode 3 (that is, $0 \leq x \leq w_p$, $y = h_p$, $L - w_e \leq z \leq L$) equal the applied voltage, $\phi = V_0$, and the interface between the PZT fiber and electrode 2 (that is, $0 \leq x \leq w_p$, $y = h_p$, $L/2 - w_e \leq z \leq L/2 + w_e$) is connected to the ground, so that $\phi = 0$. The applied electric field E_0 can be estimated to be the voltage V_0

	Elastic stiffnesses ($\times 10^{10}$ N/m ²)					Piezoelectric coefficients (C/m ²)			Dielectric constants ($\times 10^{-10}$ C/V m)	
	c_{11}	c_{33}	c_{44}	c_{12}	c_{13}	e_{31}	e_{33}	e_{15}	ϵ_{11}	ϵ_{33}
PZT-5A	12.0	11.1	2.1	7.51	7.51	-3.05	21.1	11.8	81.1	73.5

Table 1. Material properties of PZT-5A fiber.

	Young's modulus E ($\times 10^{10}$ N/m ²)	Poisson's ratio ν
Epoxy	0.29	0.30
Copper	11.7	0.31
Kapton	0.28	0.30

Table 2. Material properties of nonpiezoelectric constituents.

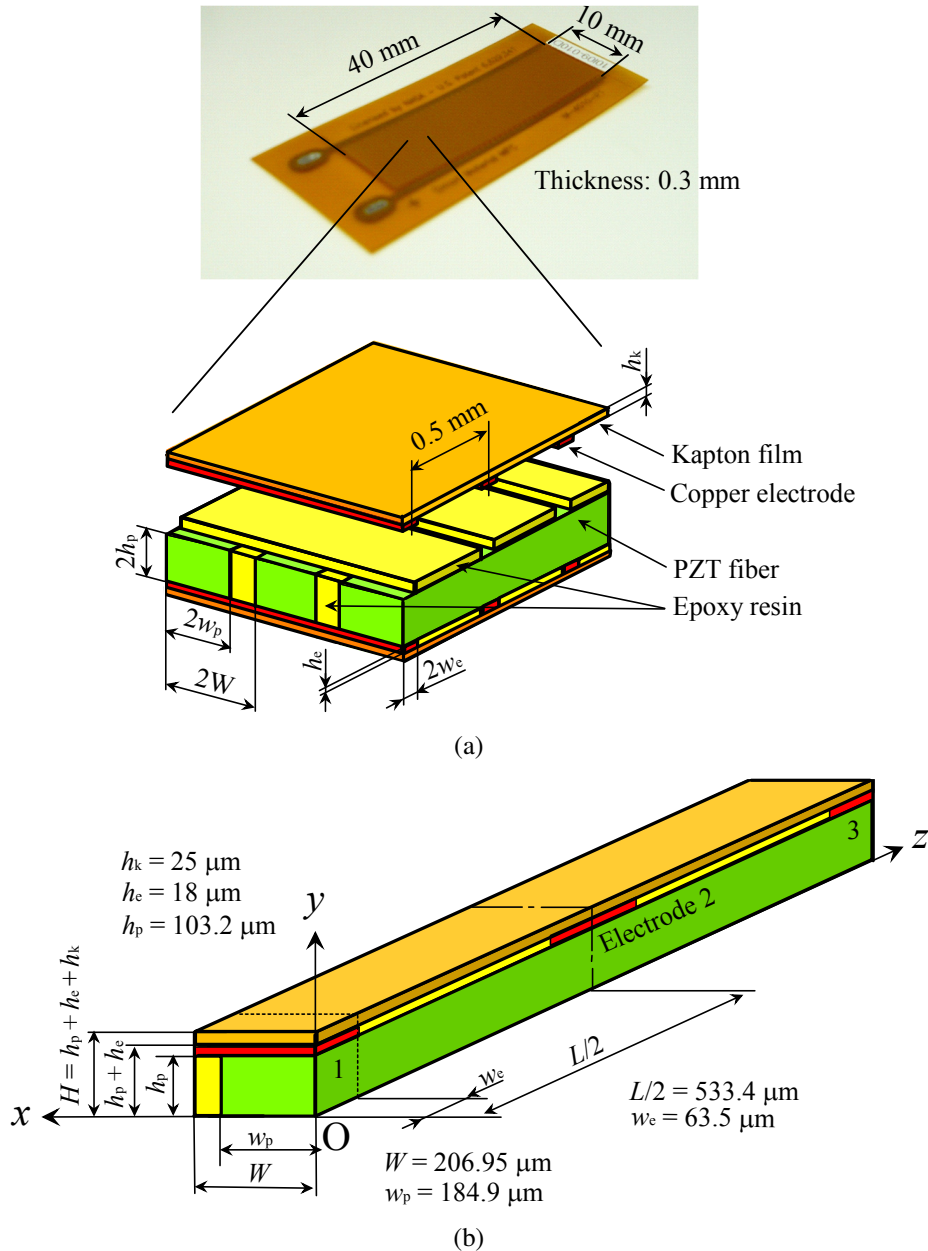


Figure 1. Schematic drawing of MFC: (a) lay-up and geometry and (b) repeating unit.

divided by the IDE spacing $L/2$. The mechanical boundary conditions include the traction-free condition on the top surface at $y = H$ and the zero-displacement conditions on the $x = 0$, $y = 0$, and $z = 0$ faces. Also included are the symmetry conditions on the side surfaces at $x = W$ and $z = L$.

Consider two types of poling. The first is partially poled. For partially poled PZT fibers, a matrix of crystalline grains with an idealized microstructure [Dent et al. 2007] is first considered, where each grain has a random polarization obtained using statistical procedures [Swain and Swain 1980]. The resulting

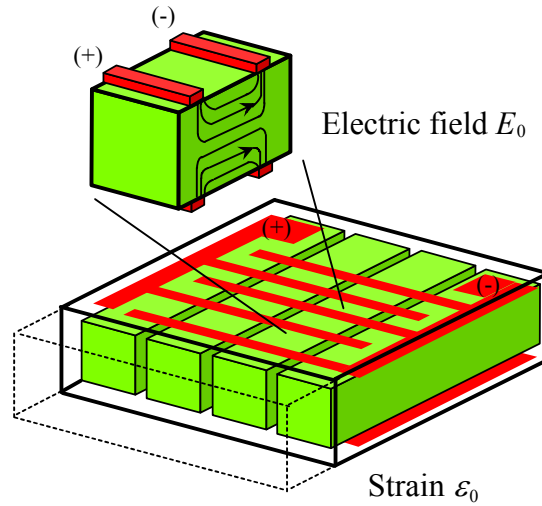


Figure 2. Strain and electric field of MFC with IDE.

material is equivalent to an unpoled piezoelectric [Shindo et al. 2009]. Figure 3a shows a typical model ($x = 0$ plane) with a fine microstructure. The grain polarizations are quantized to just six orientations, corresponding to the two directions along the three principal axes. Other directions are not considered here for simplicity. High voltage is next applied through finite element analysis (FEA), and the PZT fiber model is partially polarized. The second has fully poled PZT fibers (see Figure 3b).

Each element consists of many grains, and each grain is modeled as a uniformly polarized cell that contains a single domain. The model neglects domain wall effects and interaction among different domains. In reality, this is not true, but the assumption does not affect the macroscopic behavior of the MFC. The polarization switching is defined for each element. The voltage V_0 is applied, and the

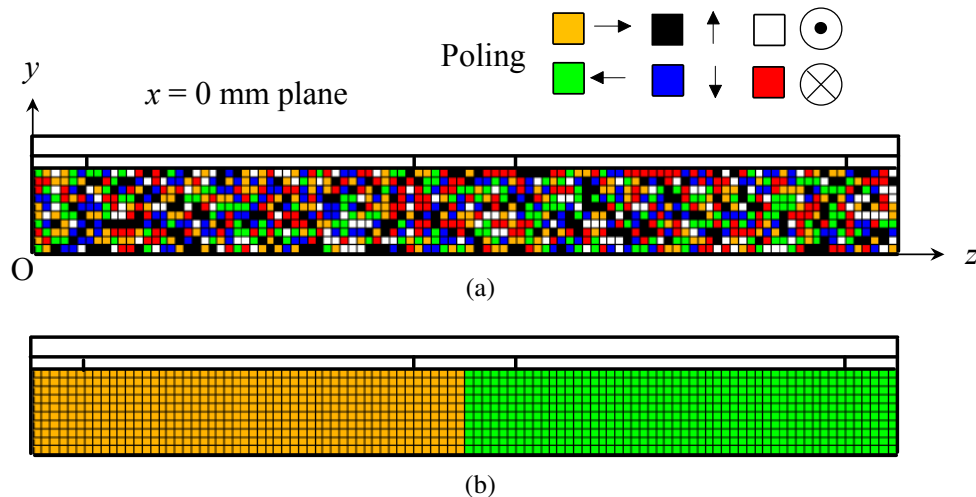


Figure 3. Models of (a) unpoled and (b) fully poled PZT fibers.

electromechanical fields of each element are computed from the FEA. The switching criterion of (5) is checked for every element to see if switching will occur. After all possible polarization switches have occurred, the piezoelectricity tensor of each element is rotated to the new polarization direction. The electromechanical fields are recalculated, and the process is repeated until the solution converges. The macroscopic response of the MFC is determined by the finite element model.

The finite element computations by ANSYS were provided by modifying the program with routines developed in our previous work (for example, [Shindo et al. 2004]). The spontaneous polarization P^s and strain γ^s were assigned representative values of 0.3 C/m^2 and 0.004 , respectively, based on the experimental data [Hwang et al. 1995]. Simulations were also run with the spontaneous polarization and strain values varying, though the results are not shown here since changing these values did not impact the results. Each element was defined by an eight-node 3D coupled field solid for the PZT fiber and an eight-node 3D structural solid for the epoxy matrix, Kapton film, and copper electrodes.

The strain ε_0^e of the repeating unit for the fully poled PZT fiber under stress-free conditions is related to the electric field E_0 by the expression [Deraemaeker et al. 2009]:

$$\varepsilon_0^e = d_{33}^e E_0. \quad (7)$$

Here, the effective longitudinal piezoelectric coefficient d_{33}^e is obtained, using microelectromechanics models based on the uniform field assumptions [Tan and Tong 2001]. Assuming that 90° switching does not occur, the effective coefficient for the repeating unit without Kapton film or copper/epoxy layer is given by

$$d_{33}^e = \begin{cases} e_{31}^e s_{13}^e + e_{32}^e s_{23}^e + e_{33}^e s_{33}^e & \text{if } E_0 > -E_c, \\ -(e_{31}^e s_{13}^e + e_{32}^e s_{23}^e + e_{33}^e s_{33}^e) & \text{if } E_0 \leq -E_c, \end{cases} \quad (8)$$

where e_{31}^e , e_{32}^e , e_{33}^e , s_{13}^e , s_{23}^e , and s_{33}^e are given in Appendix D.

3. Experimental procedure

The free strain (ε) response of the M-4010-P1 MFC (see Figure 1a) was measured. Strain gages were bonded symmetrically at the center of the active area on both sides of the piezoelectric MFC. Voltage was applied using a power supply for voltages up to 1.25 kV/DC in order to generate the strain versus electric field curve. A plot of applied voltage versus time during the test is shown in Figure 4. The MFC

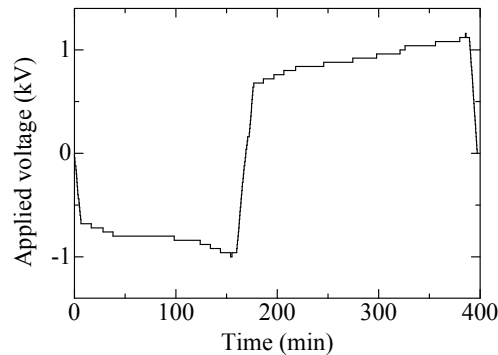


Figure 4. Applied voltage versus time.

was then cut and observed using a digital microscope. The measured entities were statistically analyzed to obtain realistic geometrical parameters. The main values are represented in Figure 1b.

4. Results and discussion

Figure 5 shows the FEA results for the distribution of poled areas at the $x = 0$ mm plane for the PZT fiber under the electric field for $E_0 = E_c = 1.5$ MV/m and for $E_0 = 2E_c = 3$ MV/m. The unpoled areas are observed under the coercive electric field. Moreover, at an electric field of $2E_c$, there are some areas where the pole is not aligned. Figure 6 provides the strain versus electric field for the piezoelectric MFCs. The solid and dot-dashed lines represent the strain ε_{zz} at $x = 0, y = H,$ and $z = 0$ for MFCs with partially and fully poled PZT fibers from the FEA while the open circle represents the test data ε . The partially poled PZT fiber is obtained under $E_0 = 2E_c$ (see Figure 5b). Also shown is the analytical data ε_0^e obtained from the microelectromechanics models (dashed line). The FEA results show that as the electric field E_0

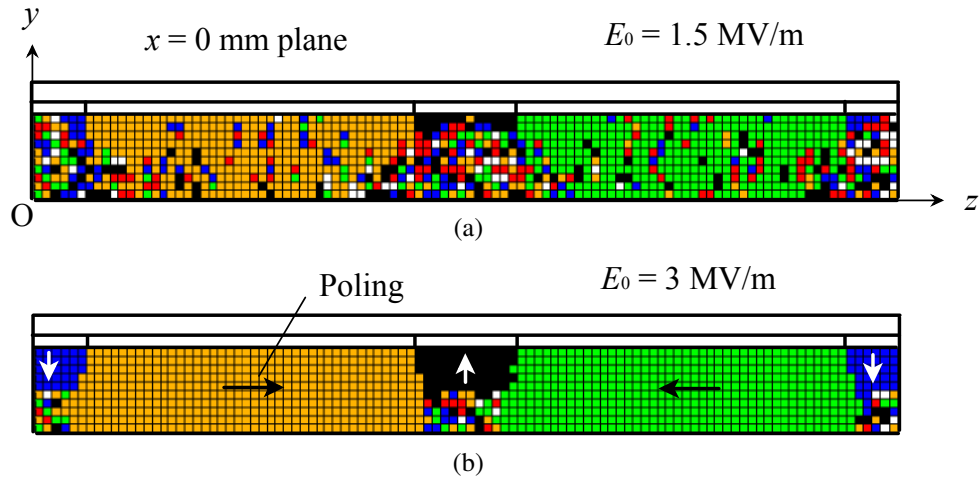


Figure 5. Images of poling for PZT fiber at (a) $E_0 = E_c = 1.5$ MV/m and (b) $E_0 = 2E_c = 3$ MV/m.

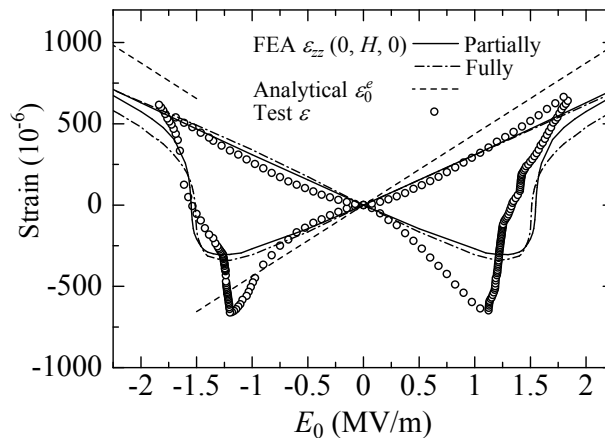


Figure 6. Strain versus electric field for piezoelectric MFCs.

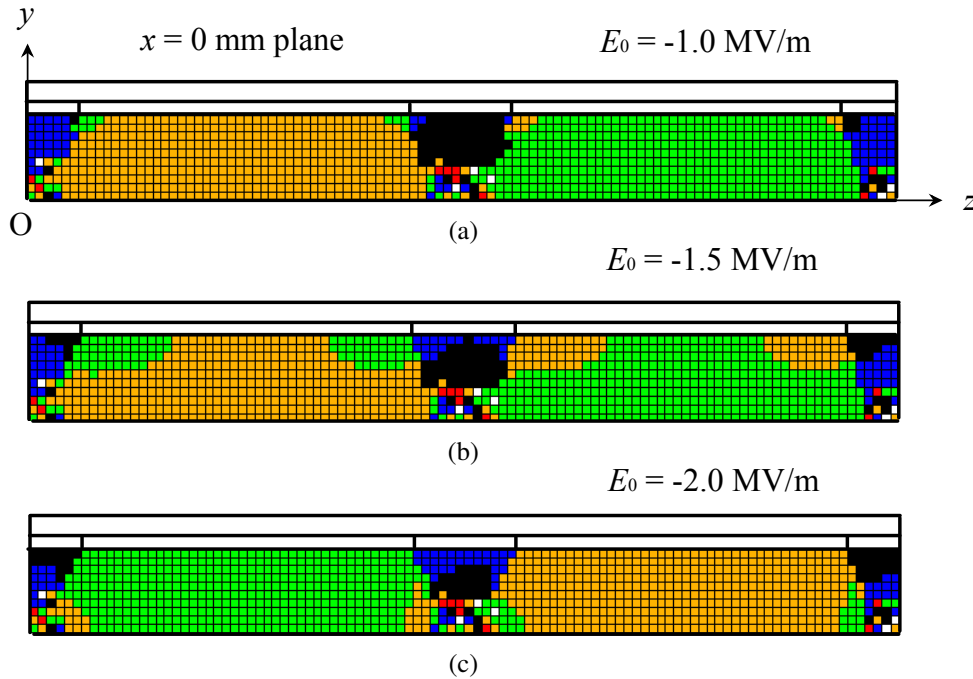


Figure 7. Polarization switching zone induced by electric field of (a) $E_0 = -1.0$ MV/m, (b) $E_0 = -1.5$ MV/m, and (c) $E_0 = -2.0$ MV/m at the $x = 0$ mm plane for MFC with partially poled PZT fibers.

is increased from zero initially, the tensile strain increases linearly due to the piezoelectric effect. On the other hand, the compressive strain increases nonlinearly as the electric field is lowered from zero; then, the compressive strain reaches maximum at about $E_0 = -1.25$ MV/m as localized depolarization occurs. The compressive strain then decreases, and the tensile strain rises as the negative remanent polarization develops. As polarization reversal takes place, the piezoelectric coefficients of the PZT fiber change their signs. This leads to a reversal of the macroscopic piezoelectric effect. The tensile strain decreases as the negative electric field is gradually decreased. As the electric field is cycled, the butterfly loop is repeated. Note that there is a good agreement between the FEA and the test. Also, little difference in the strain versus electric field curve is observed between the MFCs with partially and fully poled PZT fibers. Although the strain obtained from the microelectromechanics models is larger than that from the FEA due to neglecting the Kapton film and copper/epoxy layer, the microelectromechanics models may serve to predict roughly the strain response of the MFCs. Figure 7 shows the polarization switching zones at the $x = 0$ mm plane of the MFC with partially poled PZT fibers. The original poled state is shown in Figure 5b. Under the electric field, $E_0 = -1.0$ MV/m, below the coercive field strength $E_c = 1.5$ MV/m, polarization switching occurs near the IDE tip. It seems that the switching expands along the region near the interface between the PZT fiber and epoxy layer. The size of the 180° switching zone increases with increasing electric field opposite to the original poling direction. The above numerical and experimental results show that if MFCs are operated under negative electric fields, the polarization switching effect is by no means negligible, and designers need to be aware of the nonlinear behavior.

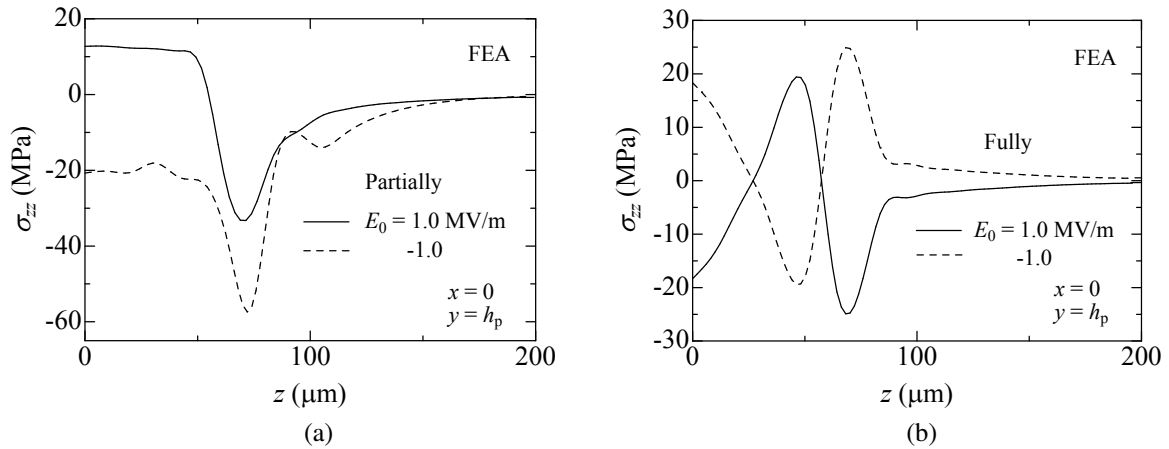


Figure 8. Variation of normal stress σ_{zz} as a function of z for MFCs with (a) partially and (b) fully poled PZT fibers; $x = 0$ mm and $y = h_p$.

The normal stress σ_{zz} as a function of z at the $x = 0$ mm plane of the MFC with partially poled PZT fibers is shown in Figure 8a for $y = h_p$ under an electric field $E_0 = \pm 1.0$ MV/m. When a positive E_0 of 1.0 MV/m is applied, the normal stress in the neighborhood of the IDE tip changes from tensile to compressive and the maximum value of the compressive stress occurs at about $z = 70$ μm . It is interesting to note that under $E_0 = -1.0$ MV/m, the highest compressive stress occurs at about $z = 75$ μm . Figure 8b shows similar results for the MFC with fully poled PZT fibers. The maximum values of the compressive and tensile stresses occur under $E_0 = 1.0$ and -1.0 MV/m, respectively, at about $z = 70$ μm . Figure 9 shows the shear stress σ_{yz} as a function of z at the $x = 0$ mm plane of the MFCs with partially and fully poled PZT fibers for $y = h_p$ under an electric field $E_0 = 1.0$ MV/m. The peak values of σ_{yz} for the MFCs with partially and fully poled PZT fibers occur at different locations, and the maximum shear stress for the MFC with partially poled PZT fibers is larger than that for the MFC with fully poled PZT fibers. Figure 10 shows the normal stress σ_{yy} as a function of z at the $x = 0$ mm plane of the MFCs with

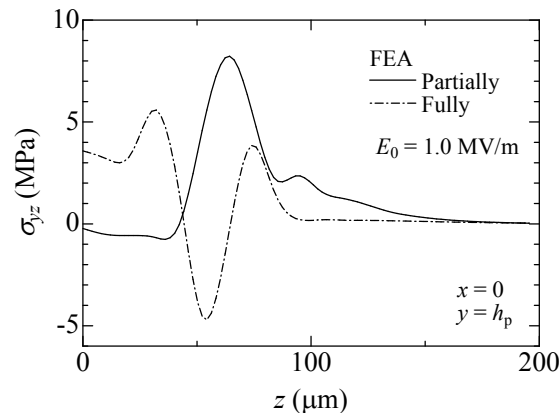


Figure 9. Variation of shear stress σ_{yz} as a function of z for MFCs with partially and fully poled PZT fibers; $x = 0$ mm and $y = h_p$.

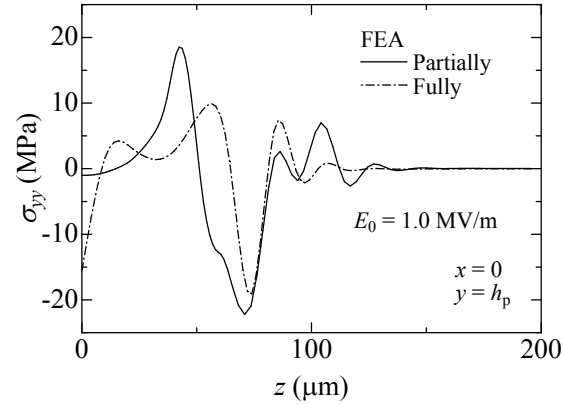


Figure 10. Variation of normal stress σ_{yy} as a function of z for MFCs with partially and fully poled PZT fibers; $x = 0$ mm and $y = h_p$.

partially and fully poled PZT fibers for $y = h_p$ under an electric field $E_0 = 1.0$ MV/m. The maximum value of the tensile stress for the MFC with partially poled PZT fibers is about twice that for the MFC with fully poled PZT fibers. A comparison between the results for MFCs with partially and fully poled PZT fibers indicates that the inhomogeneity near the IDE of the MFC has little effect on the strain versus electric field curve but affects the internal stresses.

5. Conclusions

This paper presents the results of numerical and experimental study in piezoelectric macrofiber composites (MFCs). The developed finite element model quantitatively predicted the strain versus electric field curve and captured the nonlinear electromechanical phenomena. We showed that the inhomogeneity near the interdigitated electrode (IDE) tip in the MFCs leads to dramatic differences in the internal stresses. By knowing how the partially poled lead zirconate titanate (PZT) fiber, IDE, and matrix constituents interact, we can design a MFC to achieve particular overall properties. The results of this study will help to offer a basis for optimizing piezoelectric MFC performance by selecting the optimal microstructure and properties of composite constituents.

Appendix A

For piezoelectric ceramics which exhibit hexagonal crystal symmetry of class 6 mm with respect to the principal x_1 , x_2 , and x_3 axes, the constitutive relations can be written in the form

$$\begin{Bmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \\ \sigma_4 \\ \sigma_5 \\ \sigma_6 \end{Bmatrix} = \begin{bmatrix} c_{11} & c_{12} & c_{13} & 0 & 0 & 0 \\ c_{12} & c_{11} & c_{13} & 0 & 0 & 0 \\ c_{13} & c_{13} & c_{33} & 0 & 0 & 0 \\ 0 & 0 & 0 & c_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & c_{44} & 0 \\ 0 & 0 & 0 & 0 & 0 & c_{66} \end{bmatrix} \begin{Bmatrix} \varepsilon_1 - \varepsilon_1^r \\ \varepsilon_2 - \varepsilon_2^r \\ \varepsilon_3 - \varepsilon_3^r \\ \varepsilon_4 - \varepsilon_4^r \\ \varepsilon_5 - \varepsilon_5^r \\ \varepsilon_6 - \varepsilon_6^r \end{Bmatrix} - \begin{bmatrix} 0 & 0 & e_{31} \\ 0 & 0 & e_{31} \\ 0 & 0 & e_{33} \\ 0 & e_{15} & 0 \\ e_{15} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} E_1 \\ E_2 \\ E_3 \end{Bmatrix}, \quad (\text{A.1})$$

$$\begin{Bmatrix} D_1 \\ D_2 \\ D_3 \end{Bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 0 & e_{15} & 0 \\ 0 & 0 & 0 & e_{15} & 0 & 0 \\ e_{31} & e_{31} & e_{33} & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} \varepsilon_1 - \varepsilon_1^r \\ \varepsilon_2 - \varepsilon_2^r \\ \varepsilon_3 - \varepsilon_3^r \\ \varepsilon_4 - \varepsilon_4^r \\ \varepsilon_5 - \varepsilon_5^r \\ \varepsilon_6 - \varepsilon_6^r \end{Bmatrix} + \begin{bmatrix} \epsilon_{11} & 0 & 0 \\ 0 & \epsilon_{11} & 0 \\ 0 & 0 & \epsilon_{33} \end{bmatrix} \begin{Bmatrix} E_1 \\ E_2 \\ E_3 \end{Bmatrix} + \begin{Bmatrix} P_1^r \\ P_2^r \\ P_3^r \end{Bmatrix}, \quad (\text{A.2})$$

where

$$\sigma_1 = \sigma_{11}, \sigma_2 = \sigma_{22}, \quad \sigma_3 = \sigma_{33}, \quad \sigma_4 = \sigma_{23} = \sigma_{32}, \quad \sigma_5 = \sigma_{31} = \sigma_{13}, \quad \sigma_6 = \sigma_{12} = \sigma_{21}, \quad (\text{A.3})$$

$$\varepsilon_1 = \varepsilon_{11}, \varepsilon_2 = \varepsilon_{22}, \quad \varepsilon_3 = \varepsilon_{33}, \quad \varepsilon_4 = 2\varepsilon_{23} = 2\varepsilon_{32}, \quad \varepsilon_5 = 2\varepsilon_{31} = 2\varepsilon_{13}, \quad \varepsilon_6 = 2\varepsilon_{12} = 2\varepsilon_{21}, \quad (\text{A.4})$$

$$\varepsilon_1^r = \varepsilon_{11}^r, \varepsilon_2^r = \varepsilon_{22}^r, \quad \varepsilon_3^r = \varepsilon_{33}^r, \varepsilon_4^r = 2\varepsilon_{23}^r = 2\varepsilon_{32}^r, \quad \varepsilon_5^r = 2\varepsilon_{31}^r = 2\varepsilon_{13}^r, \quad \varepsilon_6^r = 2\varepsilon_{12}^r = 2\varepsilon_{21}^r, \quad (\text{A.5})$$

$$c_{11} = c_{1111} = c_{2222}, c_{12} = c_{1122}, \quad c_{13} = c_{1133} = c_{2233}, c_{33} = c_{3333}, \quad (\text{A.6})$$

$$c_{44} = c_{2323} = c_{3131}, c_{66} = c_{1212} = \frac{1}{2}(c_{11} - c_{12}),$$

$$e_{15} = e_{131} = e_{223}, \quad e_{31} = e_{311} = e_{322}, \quad e_{33} = e_{333}. \quad (\text{A.7})$$

The remanent strain and polarization are present in the piezoelectric material poled in the positive x_3 -direction but because the remanent state is the reference for the measurement of strain and polarization, ε_{ij}^r and P_i^r are numerically equal to zero for the polarized state.

Appendix B

The values of $\Delta\varepsilon_{ij} = \varepsilon_{ij}^r$ and $\Delta P_i = P_i^r$ for 180° switching can be expressed as

$$\Delta\varepsilon_{11} = 0, \quad \Delta\varepsilon_{22} = 0, \quad \Delta\varepsilon_{33} = 0, \quad \Delta\varepsilon_{12} = 0, \quad \Delta\varepsilon_{23} = 0, \quad \Delta\varepsilon_{31} = 0, \quad (\text{B.1})$$

$$\Delta P_1 = 0, \quad \Delta P_2 = 0, \quad \Delta P_3 = -2P^s. \quad (\text{B.2})$$

For 90° switching in the x_3x_1 plane, the changes are

$$\Delta\varepsilon_{11} = \gamma^s, \quad \Delta\varepsilon_{22} = 0, \quad \Delta\varepsilon_{33} = -\gamma^s, \quad \Delta\varepsilon_{12} = 0, \quad \Delta\varepsilon_{23} = 0, \quad \Delta\varepsilon_{31} = 0, \quad (\text{B.3})$$

$$\Delta P_1 = \pm P^s, \quad \Delta P_2 = 0, \quad \Delta P_3 = -P^s, \quad (\text{B.4})$$

where γ^s is a spontaneous strain. For 90° switching in the x_2x_3 plane, we have

$$\Delta\varepsilon_{11} = 0, \quad \Delta\varepsilon_{22} = \gamma^s, \quad \Delta\varepsilon_{33} = -\gamma^s, \quad \Delta\varepsilon_{12} = 0, \quad \Delta\varepsilon_{23} = 0, \quad \Delta\varepsilon_{31} = 0, \quad (\text{B.5})$$

$$\Delta P_1 = 0, \quad \Delta P_2 = \pm P^s, \quad \Delta P_3 = -P^s. \quad (\text{B.6})$$

Appendix C

The new piezoelectric constant e'_{ikl} is related to the elastic and direct piezoelectric constants by

$$\begin{aligned}
e'_{111} &= d'_{111}c_{11} + d'_{122}c_{12} + d'_{133}c_{13}, & e'_{122} &= d'_{111}c_{12} + d'_{122}c_{11} + d'_{133}c_{13}, \\
e'_{133} &= d'_{111}c_{13} + d'_{122}c_{13} + d'_{133}c_{33}, & e'_{123} &= 2d'_{123}c_{44}, & e'_{131} &= 2d'_{131}c_{44}, & e'_{112} &= 2d'_{112}c_{66}, \\
e'_{211} &= d'_{211}c_{11} + d'_{222}c_{12} + d'_{233}c_{13}, & e'_{222} &= d'_{211}c_{12} + d'_{222}c_{11} + d'_{233}c_{13}, \\
e'_{233} &= d'_{211}c_{13} + d'_{222}c_{13} + d'_{233}c_{33}, & e'_{223} &= 2d'_{223}c_{44}, & e'_{231} &= 2d'_{231}c_{44}, & e'_{212} &= 2d'_{212}c_{66}, \\
e'_{311} &= d'_{311}c_{11} + d'_{322}c_{12} + d'_{333}c_{13}, & e'_{322} &= d'_{311}c_{12} + d'_{322}c_{11} + d'_{333}c_{13}, \\
e'_{333} &= d'_{311}c_{13} + d'_{322}c_{13} + d'_{333}c_{33}, & e'_{323} &= 2d'_{323}c_{44}, & e'_{331} &= 2d'_{331}c_{44}, & e'_{312} &= 2d'_{312}c_{66}.
\end{aligned} \tag{C.1}$$

The components of the piezoelectricity tensor d'_{ikl} are

$$d'_{ikl} = \{d_{333}n_i n_k n_l + d_{311}(n_i \delta_{kl} - n_i n_k n_l) + d_{131}(\delta_{ik} n_l - 2n_i n_k n_l + \delta_{il} n_k)\}, \tag{C.2}$$

where n_i is the unit vector in the poling direction, δ_{ij} is the Kronecker delta, $d_{333} = d_{33}$, $d_{311} = d_{31}$, and $d_{131} = d_{15}/2$ are the direct piezoelectric constants, and

$$d_{33} = \frac{(c_{11} + c_{12})e_{33} - 2c_{13}e_{31}}{\{(c_{11} + c_{12})c_{33} - 2c_{13}^2\}}, d_{31} = \frac{c_{33}e_{31} - c_{13}e_{33}}{\{(c_{11} + c_{12})c_{33} - 2c_{13}^2\}}, d_{15} = \frac{e_{15}}{c_{44}}. \tag{C.3}$$

Appendix D

In (8), e_{31}^e , e_{32}^e , e_{33}^e , s_{13}^e , s_{23}^e , and s_{33}^e are

$$e_{31}^e = e_{31} \frac{c_{11m} w_p / W}{c_{11m} w_p / W + c_{11}(1 - w_p / W)}, \tag{D.1}$$

$$e_{32}^e = e_{31}^e \frac{c_{11m} w_p / W + (c_{11} - c_{12} + c_{12m})(1 - w_p / W)}{c_{11m}}, \tag{D.2}$$

$$e_{33}^e = e_{33} w_p / W + e_{31}^e \frac{(c_{12m} - c_{13})(1 - w_p / W)}{c_{11m}}, \tag{D.3}$$

$$s_{13}^e = \frac{C_{12}C_{23} - C_{13}C_{22}}{(C_{11}C_{22} - C_{12}^2)C_{33} - C_{11}C_{23}^2 + 2C_{12}C_{13}C_{23} - C_{13}^2C_{22}}, \tag{D.4}$$

$$s_{23}^e = \frac{C_{12}C_{13} - C_{11}C_{23}}{(C_{11}C_{22} - C_{12}^2)C_{33} - C_{11}C_{23}^2 + 2C_{12}C_{13}C_{23} - C_{13}^2C_{22}}, \tag{D.5}$$

$$s_{33}^e = \frac{C_{11}C_{22} - C_{12}^2}{(C_{11}C_{22} - C_{12}^2)C_{33} - C_{11}C_{23}^2 + 2C_{12}C_{13}C_{23} - C_{13}^2C_{22}}, \tag{D.6}$$

where

$$C_{11} = \frac{c_{11}c_{11m}}{c_{11m}w_p/W + c_{11}(1 - w_p/W)}, \quad (D.7)$$

$$C_{12} = \frac{c_{12}c_{11m}w_p/W + c_{11}c_{12m}(1 - w_p/W)}{c_{11m}w_p/W + c_{11}(1 - w_p/W)}, \quad (D.8)$$

$$C_{13} = \frac{c_{13}c_{11m}w_p/W + c_{11}c_{12m}(1 - w_p/W)}{c_{11m}w_p/W + c_{11}(1 - w_p/W)}, \quad (D.9)$$

$$C_{22} = c_{11}w_p/W + c_{11m}(1 - w_p/W) + \frac{C_{12}^2}{C_{11}} - \left\{ \frac{c_{12}^2 w_p/W}{c_{11}} + \frac{c_{12m}^2(1 - w_p/W)}{c_{11m}} \right\}, \quad (D.10)$$

$$C_{23} = c_{13}w_p/W + c_{12m}(1 - w_p/W) + \frac{C_{12}C_{13}}{C_{11}} - \left\{ \frac{c_{12}c_{13}w_p/W}{c_{11}} + \frac{c_{12m}^2(1 - w_p/W)}{c_{11m}} \right\}, \quad (D.11)$$

$$C_{33} = c_{33}w_p/W + c_{11m}(1 - w_p/W) + \frac{C_{13}^2}{C_{11}} - \left\{ \frac{c_{13}^2 w_p/W}{c_{11}} + \frac{c_{12m}^2(1 - w_p/W)}{c_{11m}} \right\}, \quad (D.12)$$

and

$$c_{11m} = \frac{E_m(1 - \nu_m)}{(1 + \nu_m)(1 - 2\nu_m)}, \quad c_{12m} = \frac{E_m\nu_m}{(1 + \nu_m)(1 - 2\nu_m)}. \quad (D.13)$$

E_m and ν_m in (D.13) are the Young's modulus and Poisson's ratio of the epoxy matrix.

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